## 1145 Fuller Avenue

## Town of Penetanguishene

Traffic Impact Study for Tonking Management Inc.

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JD Northcote Engineering Inc.
86 Cumberland Street
Barrie, ON
705.725.4035

ENGINEERING

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## Executive Summary

This report summarizes the traffic impact study prepared for the proposed mixed-use development municipally known as 1145 Fuller Avenue located in the southwest corner of the of the Pine Grove Road / Fuller Avenue intersection in the Town of Penetanguishene [Town], County of Simcoe [County]. The report assesses the impact of traffic related to the development on the adjacent roadway and provides recommendations to accommodate this traffic in a safe and efficient manner.

The proposed residential development includes a 0.56 acre commercial block, 102 residential single detached units, 86 residential townhouse units and a 0.56 acre residential multi-density block. The specifics of the residential multi-density lands are currently unknown; however, based on discussions with the developer, it is anticipated there will be a maximum of 20 residential units. Similarly, the specifics for the development of the commercial block are not known at this time. A supplemental transportation analysis for the residential multi-density block and the commercial block will be provided at a later date, if necessary.

The proposed development will have one full-movement access driveway onto Pine Grove Road [North Access] and one full-movement access driveway onto Fuller Avenue [South Access]. For the purpose of this analysis, we have assumed one full-movement access driveway onto Fuller Avenue [Commercial Access] from the commercial block.

The scope of this analysis includes a review of the following intersections:

- Pine Grove Road \& Sheffcote Street / Fuller Avenue;
- Robert Street East / Fuller Avenue;
- Pine Grove Road / North Access;
- Commercial Access / Fuller Avenue;
- South Access / Fuller Avenue; and
- Robert Street East / Thompsons Road \& Centennial Drive.


## Conclusions

1. The proposed development is expected to generate a total of 140 AM peak hour trips and 204 PM peak hour trips.
2. Detailed turning movement counts were completed for all existing intersections on Tuesday, November $6{ }^{\text {th }}, 2018$.
3. An intersection operation analysis was completed at the study area intersections, using the existing (2018) and background (2028) traffic volumes, with the adjacent development traffic and without the proposed development traffic. This enabled a review of existing and future traffic deficiencies that would be present without the influence of the proposed development. The following transportation infrastructure improvements are recommended:

## Fuller Avenue / Robert Street East

Background (2028) Traffic Volumes

- Signalization of intersection;
- Northbound left turn auxiliary lane;
- ( 45 metre storage length and 55 metre taper length)
- Southbound right turn auxiliary lane;
- (30 metre storage length and 60 metre taper length)
- Eastbound right turn auxiliary lane.
- ( 30 metre storage length and 30 metre taper length)

4. An estimate of the amount of traffic that would be generated by the proposed development was prepared and assigned to the study area streets and intersections.
5. An intersection operation analysis was completed under total (2028) traffic volumes with the proposed development operational at the study area intersections. No additional infrastructure improvements are recommended.
6. The proposed South Access and Commercial Access driveways will operate efficiently as full movement access driveways with one-way stop control for westbound traffic. The proposed North Access driveway will operate efficiently as a full movement access driveway with one-way stop control for northbound traffic. A single lane for ingress and egress movements at the South Access, Commercial Access and North Access will provide the necessary capacity to convey the traffic volume generated by the proposed development.
7. The sight distance available for the proposed South Access and North Access meets the minimum stopping sight distance requirements. The sight distance available for the Commercial Access has not been analysed in this study as the specifics of the proposed development commercial block access driveways are currently unknown.
8. In summary, the proposed development will not cause any operational issues and will not add a notable delay or congestion to the local roadway network.

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## 1 Introduction

### 1.1 Background

Tonking Management Inc. [The Developer] is proposing a mixed-use development on the property municipally known as 1145 Fuller Avenue, located in the southwest corner of the of the Pine Grove Road / Fuller Avenue intersection in the Town of Penetanguishene [Town], County of Simcoe [County].

The proposed residential development includes a 0.56 acre commercial block, 102 residential single detached units, 86 residential townhouse units and a 0.56 acre residential multi-density block. The specifics of the residential multi-density lands are currently unknown; however, based on discussions with the developer, it is anticipated there will be a maximum of 20 residential units. Similarly, the specifics for the development of the commercial block are not known at this time. A supplemental transportation analysis for the residential multi-density block and the commercial block will be provided at a later date, if necessary.

The proposed development will have one full-movement access driveway onto Pine Grove Road [North Access] and one full-movement access driveway onto Fuller Avenue [South Access]. For the purpose of this analysis, we have assumed one full-movement access driveway onto Fuller Avenue [Commercial Access] from the commercial block.

The Developer has retained JD Northcote Engineering Inc. [JD Engineering] to prepare this traffic impact study in support of the proposed development.

### 1.2 Study Area

Figure 1 shows the location of the proposed development and study area intersections, in relation to the surrounding area. The Site Plan by Innovative Planning Solutions is provided in Appendix A.

The proposed development is bound by Fuller Avenue to the west, existing residential lands to the south, environmentally protected lands to the east and Pine Grove Road to the north.

Through consultation with the Town, the following intersections are included in the traffic impact study:

- Pine Grove Road \& Sheffcote Street / Fuller Avenue;
- Robert Street East / Fuller Avenue;
- Pine Grove Road / North Access;
- Commercial Access / Fuller Avenue;
- South Access / Fuller Avenue; and
- Robert Street East / Thompsons Road \& Centennial Drive.

Figure 1 - Proposed Site Location and Study Area


### 1.3 Study Scope and Objectives

The purpose of this study is to identify the potential impacts to traffic flow at the site access and on the surrounding roadway network. The study analysis includes the following tasks:

- Consult with the Town to address any traffic-related issues or concerns they have with the proposed development;
- Determine existing traffic volumes and circulation patterns;
- Estimate future traffic volumes if the proposed development was not constructed, including the impact of additional proposed developments in the area;
- Complete level-of-service [LOS] analysis of horizon year (without the proposed development) traffic conditions and identify operational deficiencies;
- Estimate the amount of traffic that would be generated by the proposed development and assign to the roadway network;
- Complete LOS analysis of horizon year (with the proposed development) traffic conditions and identify additional operational deficiencies;
- Identify improvement options to address operational deficiencies; and
- Document findings and recommendations in a final report.


### 1.4 Horizon Year and Analysis Periods

Traffic scenarios for the existing year (2018) and 10-year (2028) horizon year were selected for analysis of traffic operations in the study area. The weekday morning [AM] and weekday afternoon [PM] peak hours have been selected as the analysis periods for this study.

## 2 Information Gathering

### 2.1 Street and Intersection Characteristics

Fuller Avenue is a two-lane major arterial road with a rural cross-section, within the study area. Fuller Avenue has an asphalt shoulder on both sides of the road, north of Pine Grove Road, an asphalt shoulder on the west side of the road and a gravel shoulder on the east side of the road between Pine Grove Road and Cambridge Street, and a gravel shoulder on both sides of the road south of Cambridge Street. Fuller Avenue has a posted speed limit of $60 \mathrm{~km} / \mathrm{h}$ and is under the jurisdiction of the Town.

Robert Street East is a two-lane major arterial road with a rural cross section and a gravel shoulder on both sides of the road, within the study area. Robert Street East has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$ and is under the jurisdiction of the Town, within the study area.

Thompsons Road is a two-lane collector road with a rural cross section and a gravel shoulder on both sides of the road, within the study area. Thompsons Road has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$ and is under the jurisdiction of the Town.

Centennial Drive is a two-lane local road with a rural cross section. Centennial Drive has an assumed (unposted) speed limit of $50 \mathrm{~km} / \mathrm{h}$ and is under the jurisdiction of the Town.

Pine Grove Road is a two-lane local road with a rural cross section. Pine Grove Road has an assumed (unposted) speed limit of $50 \mathrm{~km} / \mathrm{h}$ and is under the jurisdiction of the Town.

Sheffcote Street is a two-lane local road with a rural cross section. Sheffcote Street has an assumed (unposted) speed limit of $50 \mathrm{~km} / \mathrm{h}$ and is under the jurisdiction of the Town.

The existing intersection spacing and lane configuration within the study area is illustrated in Figure 2.

Figure 2 - Existing Intersection Spacing and Lane Configuration with in Study Area


### 2.2 Local Transportation Infrastructure Improvements

Based on discussions with the Town, there are no significant road improvements within the study area. However, it is noted that an engineering design project will be completed in 2019 by the Town for the Robert Street East / Fuller Avenue intersection to determine if intersection improvements are required.

### 2.3 Transit Access

The Penetanguishene bus route connects the Town of Penetanguishene with the Town of Midland. This bus route provides bus service to various points of interest within the Town, travelling along Fuller Avenue north of Pine Grove Road within the study area.

The Penetanguishene bus route operates between 06:30-17:30 on weekdays and 08:30-16:30 on Saturdays, with service every 60 minutes. There is no bus service on Sundays or Holidays. The closest bus stop to the proposed development for the Penetanguishene bus route is located at the Church Street / Cambridge Street intersection. It is noted that this bus route provides a "flag on" service where passengers are not required to be at a bus stop and can "flag down" the along its route to get on the bus.

### 2.4 Other Developments within the Study Area

Based on discussions with Town staff, there are two planned developments in the study area that will have a notable impact on the local traffic volumes, specifically:

- 15 Sheffcote Street; and
- 177 Robert Street East.

There is one other planned development in the study area, 948 Fuller Avenue; however, this development has not been considered in our analysis as the traffic volumes generated by this development, as identified in the Traffic Impact Assessment by C.C. Tatham and Associates Ltd., will have a negligible impact on the local traffic volumes at the study area intersections.

### 2.4.1 Traffic Generation for the 15 Sheffcote Street Development

The 15 Sheffcote Street development is located in the northwest corner of the Fuller Avenue / Pine Grove Road \& Sheffcote Street intersection and is anticipated to include 1,813 sq.ft. commercial space and two residential units. It is anticipated that this development will be fully built-out prior to the 2028 horizon year.

The traffic generation for the 15 Sheffcote Street development has been based on the Institute of Transportation Engineers [ITE] Trip Generation Manual ( $10^{\text {th }}$ Edition) [ITE Trip Generation Manual]. The following ITE land uses have been applied to estimate the traffic from the 15 Sheffcote Street development:

- ITE land use 220 (Multifamily Housing (Low-Rise)) - General Urban / Suburban Setting
- ITE land use 820 (Shopping Centre) - General Urban / Suburban Setting

The estimated trip generation of the 15 Sheffcote Street development is illustrated below in Table 1. The AM and PM peak traffic generation for the residential component of the 15 Sheffcote Street development is not expected to exactly align with the AM and PM peak hour in the traffic counts; consequently, we have applied the peak hour of adjacent street traffic values provided in the ITE Trip Generation Manual.

For the shopping centre ITE land use, the fitted curve equation for the peak hour of adjacent street traffic has been used in our calculation for the PM peak hour. It is noted this results in a conservative estimate of the trip generation, based on the size of the development. The fitted curve equation for the AM peak hour of adjacent street traffic has a low $R^{2}$ value; consequently, we have applied the more conservative average rate in our calculation for the AM peak hour.

Table 1 - Estimated Traffic Generation of the 15 Sheffcote Street Development

| Land Use | Size | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | IN | OUT | TOTAL | IN | OUT | TOTAL |
| Multifamily Housing (Low-Rise) <br> ITE Land Use: 220 | 2 units | 0 | 1 | 1 | 1 | 1 | 2 |
| Shopping Centre <br> ITE Land Use: 820 | 1,813 sq. ft. | 3 | 3 | 6 | 13 | 15 | 28 |
| TOTAL TRIP GENERATION | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{7}$ | $\mathbf{1 4}$ | $\mathbf{1 6}$ | $\mathbf{3 0}$ |  |
| PASS-BY TRIPS * |  | - | - | - | -5 | -5 | -10 |
| PRIMARY TRIPS | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{7}$ | $\mathbf{9}$ | $\mathbf{1 1}$ | $\mathbf{2 0}$ |  |

* Commercial pass-by trips for the AM and PM peak hour are 0\% and 34\% respectively, according to the ITE data for land use 820.

No transportation modal split has been applied to the above-noted traffic generation calculation.

### 2.4.2 Traffic Generation for the 177 Robert Street East Development

The 177 Robert Street East development located north of Robert Street East between Fuller Avenue and Centennial Drive, consists of an existing $1,393.5$ sq.m. facility which is to be renovated and expanded into a $4,106.5$ sq.m. manufacturing facility. It is anticipated that this development will be fully built-out prior to the 2028 horizon year.

The traffic generation for the 177 Robert Street East development has been based on the ITE Trip Generation Manual. The following ITE land use has been applied to estimate the traffic from the 177 Robert Street East development:

- ITE land use 140 (Manufacturing) - General Urban / Suburban Setting

The estimated trip generation of the 177 Robert Street East development is illustrated below in Table 2. The AM and PM peak traffic generation for the 177 Robert Street East development is not expected to exactly align with the AM and PM peak hour in the traffic counts; consequently, we have applied the peak hour of adjacent street traffic values provided in the ITE Trip Generation Manual.

Table 2 - Estimated Traffic Generation of the 177 Robert Street East development

| Land Use | Size | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | IN | OUT | TOTAL | IN | OUT | TOTAL |
| Manufacturing <br> ITE Land Use: 140 | 44,202 sq.ft. | 21 | 6 | 27 | 9 | 21 | 30 |

No transportation modal split has been applied to the above-noted traffic generation calculation.

### 2.4.3 Traffic Assignment for the 15 Sheffcote Street Development

Using the traffic distributions patterns noted in Section 4.2, the residential, commercial pass-by and commercial primary traffic assignment for the 15 Sheffcote Street Development was calculated for the AM and PM peak hour and is illustrated in Figures 3, 4 and 5 respectively.

The distribution of traffic entering at each access location is based on our review of the internal parking and building layout, in conjunction with the external traffic distribution.

### 2.4.4 Traffic Assignment for the 177 Robert Street East Development

Using the traffic distributions patterns noted in Section 4.2, the traffic assignment for the 177 Robert Street East Development was calculated for the AM and PM peak hour and is illustrated in Figure 6.

Figure 3-15 Sheffcote Street - Residential Traffic Assignment
SHEFFCOTE RD

Figure 4-15 Sheffcote Street - Commercial Pass-by Traffic Assignment
SHEFFCOTE RD

Figure 5-15 Sheffcote Street - Commercial Primary Traffic Assignment


Figure 6-177 Robert Street East - Traffic Assignment


### 2.5 Background Growth Rate

Based on discussions with the Town and to stay consistent with other recent traffic studies, a background growth rate of $2 \%$ has been selected for the study area.

### 2.6 Traffic Counts

Detailed turning movement traffic and pedestrian counts were commissioned by JD Engineering for all existing study area intersections.

Table 3 summarizes the traffic count data collection information.
Table 3 - Traffic Count Data

| Intersection <br> (N-S Street / E-w Street) | Count Date | AM Peak <br> Hour | PM Peak <br> Hour | Source |
| :---: | :---: | :---: | :---: | :---: |
| Pine Grove Road \& Sheffcote <br> Street / Fuller Avenue | Tuesday, November 6, 2018 | $07: 30-08: 30$ | $16: 00-17: 00$ | JD Eng.* |
| Robert Street East / Fuller Avenue | Tuesday, November 6, 2018 | $07: 45-08: 45$ | $16: 00-17: 00$ | JD Eng. ${ }^{*}$ |
| Robert Street East / Thompsons <br> Road \& Centennial Drive | Tuesday, November 6, 2018 | $07: 45-08: 45$ | $16: 00-17: 00$ | JD Eng.* |

*Traffic counts were completed by Accu-Traffic Inc. on behalf of JD Engineering.
Detailed traffic count data can be found in Appendix B. The peak hours of traffic generation for the study area intersections generally aligned with the anticipated peak hour of traffic generation by the proposed development. Although the AM and PM peak periods at all study area intersections did not exactly align, for the purpose of this report, we have assumed that the AM and PM peak hours are concurrent.

Heavy vehicle percentages from the traffic count data have also been included in the Synchro analysis.

Figure 7 illustrates the existing (2018) AM and PM peak hour traffic volumes within the study area.

### 2.7 Horizon Year Traffic Volumes

In addition to the adjacent development traffic volumes (outlined in Section 2.4), the background traffic growth rate discussed in Section 2.5 has also been applied to the existing traffic volumes to estimate the background (2028) horizon year traffic volumes.

Figure 8 illustrates the background (2028) horizon year AM and PM peak hour traffic volumes in the study area.

Figure 7 - Existing (2018) Traffic Volumes


Figure 8 - Background (2028) Traffic Volumes


## 3 Intersection Operation without Proposed Development

### 3.1 Introduction

Existing year operational conditions were established to determine how the street network within the study area is currently functioning without the proposed development. This provides a base case scenario to compare with future development scenarios. Traffic operations within the study area were evaluated using the 2018 traffic volumes with the existing road configuration and traffic control. The intersection performance was measured using the traffic analysis software, Synchro 10, a deterministic model that employs Highway Capacity Manual and Intersection Capacity Utilization methodologies for analyzing intersection operations. These procedures are accepted by provincial and municipal agencies throughout North America.

Synchro 10 enables the study area to be graphically defined in terms of streets and intersections, along with their geometric and traffic control characteristics. The user is able to evaluate both signalized and unsignalized intersections in relation to each other, thus not only providing level of service for the individual intersections, but also enabling an assessment of the impact the various intersections in a network have on each other in terms of spacing, traffic congestion, delay, and queuing.

Individual turning movements with a volume-to-capacity [V/C] ratio of 0.85 or greater are considered to be critical movements and have been highlighted in the LOS tables.

The intersection operations were also evaluated in terms of the LOS. LOS is a common measure of the quality of performance at an intersection and is defined in terms of vehicular delay. This delay includes deceleration delay, queue move-up time, stopped delay, and acceleration delay. LOS is expressed on a scale of A through F, where LOS A represents very little delay (i.e. less than 10 seconds per vehicle) and LOS F represents very high delay (i.e. greater than 50 seconds per vehicle for a stop sign controlled intersection and greater than 80 seconds per vehicle for a signalized intersection).

The LOS criteria for signalized and stop sign controlled intersections are shown in Table 4. A description of traffic performance characteristics is included for each LOS.

Table 4 - Level of Service Criteria for Intersections

| LOS | LOS Description | Control Delay (seconds per vehicle) |  |
| :---: | :---: | :---: | :---: |
|  |  | Signalized <br> Intersections | Stop Controlled <br> Intersections |
| A | Very low delay; most vehicles do not stop (Excellent) | less than 10.0 | less than 10.0 |
| B | Higher delay; more vehicles stop (Very Good) | between 10.0 and 20.0 | between 10.0 and 15.0 |
| C | Higher level of congestion; number of vehicles <br> stopping is significant, although many still pass <br> through intersection without stopping (Good) | between 20.0 and 35.0 | between 15.0 and 25.0 |
| D | Congestion becomes noticeable; vehicles must <br> sometimes wait through more than one red light; many <br> vehicles stop (Satisfactory) | between 35.0 and 55.0 | between 25.0 and 35.0 |
| E | Vehicles must often wait through more than one red <br> light; considered by many agencies to be the limit of <br> acceptable delay | between 55.0 and 80.0 | between 35.0 and 50.0 |
| F | This level is considered to be unacceptable to most <br> drivers; occurs when arrival flow rates exceed the <br> capacity of the intersection (Unacceptable) | greater than 80.0 | greater than 50.0 |

### 3.2 Existing (2018) Intersection Operation

The results of the LOS analysis under existing traffic volumes during the AM and PM peak hour can be found below in Table 5. Existing intersection geometry and traffic control have been utilized for this scenario. Detailed output of the Synchro analysis can be found in Appendix C.

Table 5 - Existing LOS

| Location <br> (N-S Street / E-W Street) | Weekday AM Peak Hour |  |  | Weekday PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C | Delay (s) | LOS | V/C | Delay (s) | LOS |
| Fuller Avenue / Pine Grove Road \& Sheffcote Street (unsignalized) | - | 1.7 | A | - | 1.6 | A |
| EB | 0.08 | 10.5 | B | 0.05 | 12.1 | B |
| WB | 0.09 | 16.5 | C | 0.07 | 16.2 | C |
| Thompsons Road \& Centennial Drive / Robert Street East | - | 4.5 | A | - | 5.7 | A |
| NB | 0.22 | 13.8 | B | 0.20 | 14.2 | B |
| SB | 0.13 | 15.6 | C | 0.30 | 19.9 | C |
| Fuller Avenue / Robert Street East (unsignalized) | - | 14.9 | B | - | 10.9 | C |
| EB | 0.81 | 41.1 | E | 0.74 | 36.7 | E |

The results of the LOS analysis indicate that all intersections are operating within the typical design limits noted in Section 3.1.

An analysis was completed for left turn movements at the unsignalized study area intersections, based on the criteria outlined in Appendix 9A of the Ontario Ministry of Transportation Design Supplement for TAC Geometric Design Guide for Canadian Roads June 2017 [MTO DS]. Our analysis indicates that a left turn lane is warranted in the northbound direction at the Fuller Avenue / Robert Street East intersection (results are provided in Appendix D); however, immediate reconstruction of this intersection is not recommended, based on our review of the traffic operations at this intersection, as illustrated in the Synchro analysis. A left turn lane is also warranted in the
westbound direction at the Thompsons Road \& Centennial Drive / Robert Street East intersection (results are provided in Appendix D); however, immediate reconstruction of this intersection is not recommended, based on our review of the traffic operations at this intersection, as illustrated in the Synchro analysis.

A review of the need for an auxiliary right turn lane at the unsignalized study area intersections was completed as part of our analysis. The results of the Synchro analysis indicate that there is excess capacity for all movements; consequently, an auxiliary right turn lane is not recommended. There is a high volume of southbound right turn movements at the intersection of Fuller Avenue / Robert Street East; however, immediate reconstruction of this intersection is not recommended, based on our review of the traffic operations at this intersection, as illustrated in the Synchro analysis.

Based on the Ontario Traffic Manual Book 12 Signal Justification, traffic signals are not warranted at the unsignalized study area intersections (results are provided in Appendix E).

No infrastructure improvements are recommended within the study area.

### 3.3 Background (2028) Intersection Operation

The results of the LOS analysis under background (2028) traffic volumes during the AM and PM peak hour can be found below in Table 6. Existing intersection geometry and traffic control have been utilized for this scenario. Detailed output of the Synchro analysis can be found in Appendix F.

Table 6 - Background (2028) LOS

| Location <br> (N-S Street / E-W Street) | Weekday AM Peak Hour |  |  | Weekday PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C | Delay (s) | LOS | V/C | Delay (s) | LOS |
| Fuller Avenue / Pine Grove Road \& Sheffcote Street (unsignalized) | - | 2.1 | A | - | 2.5 | A |
| EB | 0.12 | 11.5 | B | 0.14 | 14.7 | B |
| WB | 0.14 | 21.1 | C | 0.14 | 23.0 | C |
| Thompsons Road \& Centennial Drive / Robert Street East (unsignalized) | - | 5.4 | A | - | 8.1 | B |
| NB | 0.33 | 16.8 | C | 0.31 | 18.4 | C |
| SB | 0.20 | 20.0 | C | 0.52 | 34.6 | D |
| Fuller Avenue / Robert Street East (unsignalized) | - | 69.4 | C | - | 58.1 | E |
| EB | 1.36 | 216.7 | F | 1.39 | 233.1 | F |

The results of the LOS analysis indicate the intersection of Fuller Avenue / Robert Street East is operating beyond the design criteria limits specified in Section 3.1. Based on the Ontario Traffic Manual Book 12 Signal Justification, traffic signals are not warranted at the Fuller Avenue / Robert Street East intersection (results are provided in Appendix E); however, it is recommended that this intersection is reconstructed, including the installation of traffic signals in order to improve the control delay for the west approach and the overall intersection operation. It is recommended that the intersection reconstruction include the following geometric lane improvements:

- Northbound left turn auxiliary lane ( 45 metre storage length and 55 metre taper length);
- Southbound right turn auxiliary lane ( 30 metre storage length and 60 metre taper length); and
- Eastbound right turn auxiliary lane ( 30 metre storage length and 30 metre taper length).

The results of the analysis with the above-noted improvements are illustrated in Table 7 below. Detailed output of the Synchro analysis can be found in Appendix F.

Table 7 - Background (2028) LOS with Improvements

| Location <br> (N-S Street / E-W Street) | Weekday AM Peak Hour |  |  | Weekday PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C | Delay (s) | LOS | V/C | Delay (s) | LOS |
| Fuller Avenue / Robert Street East <br> (signalized) | 0.43 | 14.8 | B | 0.46 | 13.8 | B |
| EBL | 0.53 | 34.5 | C | 0.41 | 32.7 | C |
| EBR | 0.17 | 30.2 | C | 0.17 | 30.8 | C |
| NBL | 0.37 | 5.0 | A | 0.44 | 5.0 | A |
| NBT | 0.24 | 5.0 | A | 0.14 | 3.9 | A |
| SBT | 0.26 | 11.6 | B | 0.37 | 11.8 | B |
| SBR | 0.06 | 9.9 | A | 0.21 | 10.3 | B |

The results of the LOS analysis indicate that all intersections are operating within the typical design limits noted in Section 3.1.

An analysis was completed for left turn movements at the unsignalized study area intersections, based on the criteria outlined in Appendix 9A of the MTO DS. Our analysis indicates that a left turn lane is warranted in the westbound direction at the Thompsons Road \& Centennial Drive / Robert Street East intersection (results are provided in Appendix D); however, reconstruction of this intersection is not recommended for this horizon year, based on our review of the traffic operations at this intersection, as illustrated in the Synchro analysis.

A review of the need for an auxiliary right turn lane at the unsignalized study area intersections was completed as part of our analysis. The results of the Synchro analysis indicate that there is excess capacity for all movements; consequently, additional auxiliary right turn lanes are not recommended.

The anticipated $95^{\text {th }}$ percentile queue length for all auxiliary turn lanes in the study area can be accommodated by the existing auxiliary lane storage lengths.

Based on the Ontario Traffic Manual Book 12 Signal Justification, traffic signals are not warranted at the unsignalized study area intersections (results are provided in Appendix E).

## 4 Proposed Development Traffic Generation and Assignment

### 4.1 Traffic Generation

The traffic generation for the proposed development has been based on the ITE Trip Generation Manual. The following ITE land use has been applied to estimate the traffic from the proposed development:

- ITE land use 210 (Single-Family Detached Housing) - General Urban / Suburban Setting
- ITE land use 220 (Multifamily Housing (Low-Rise)) - General Urban / Suburban Setting
- ITE land use 820 (Shopping Centre) - General Urban / Suburban Setting

The estimated trip generation of the proposed development is illustrated below in Table 8. The AM and PM peak traffic generation for the residential component of the proposed development is not expected to exactly align with the AM and PM peak hour in the traffic counts; consequently, we have applied the peak hour of adjacent street traffic values provided in the ITE Trip Generation Manual.

For the shopping centre ITE land use, the fitted curve equation for the peak hour of adjacent street traffic has been used in our calculation for the PM peak hour. The fitted curve equation for the AM peak hour of adjacent street traffic has a low $R^{2}$ value; consequently, we have conservatively applied the average rate in our calculation for the AM peak hour

Table 8 - Estimated Traffic Generation of Proposed Development

| Land Use | Size | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | IN | OUT | TOTAL | IN | OUT | TOTAL |
| Single-Family Detached Housing ITE Land Use: 210 | 105 units | 20 | 59 | 78 | 66 | 38 | 104 |
| Multifamily Housing (Low-Rise) ITE Land Use: 220 | 106 units* | 11 | 38 | 49 | 38 | 22 | 60 |
| TOTAL RESIDENTIAL |  | 31 | 97 | 127 | 104 | 60 | 164 |
| Shopping Centre ITE Land Use: 820 | 22, 766 sq. ft.** | 9 | 8 | 17 | 31 | 33 | 64 |
| TOTAL TRIP GENERATION |  | 40 | 105 | 144 | 135 | 93 | 228 |
| INTERNAL CAPTURE |  | -2 | -2 | -4 | -12 | -12 | -24 |
| NET SITE GENERATION |  | 38 | 103 | 140 | 123 | 81 | 204 |
| PASS-BY TRIPS *** |  | - | - | - | -9 | -9 | 18 |
| PRIMARY TRIPS |  | 38 | 103 | 140 | 114 | 72 | 186 |

*The 106 units includes 86 townhouse units and 20 units from the residential multi-density lands
**Commercial building GFA has been calculated assuming 25\% building coverage and GLA at 90\% of GFA.
*** Commercial pass-by trips for the AM and PM peak hour are $0 \%$ and $34 \%$ respectively, according to the ITE data for ITE land use 820 .

No transportation modal split has been applied to the above-noted traffic generation calculation.

### 4.2 Traffic Assignment

For the purposes of this study, it has been assumed that all traffic generated by the proposed development will be new traffic and would not be in the study area if the development was not constructed.

The distribution of traffic entering at each access location is based on our review of the internal parking and building layout, in conjunction with the external traffic distribution.

The ITE data provides the anticipated percentage of new traffic entering and exiting during the peak hour. The distribution of residential traffic has been calculated based on the 2016 Transportation Tomorrow Survey [TTS] data for traffic zone 8573, retrieved using the TTS Internet Data Retrieval System [IDRS] (output attached as Appendix G). TTS data provides historical origin and destination work trip percentages for specific areas within the Town and southern Ontario.

Traffic distribution for the trips generated by the residential component of the proposed development during the AM and PM peak hour is expected to generally follow commuter travel patterns. Our analysis is based on egress traffic during the AM peak hour. Logically, the distribution of ingress traffic will follow the inverse of the exiting traffic distribution. For each of the individual areas identified in the TTS data, we have selected the probable route of travel, assuming that people will select their route primarily based on travel time.

The distribution of trips is illustrated in Table 9 using the methodology outlined above.

Table 9 - Proposed Development Residential Traffic Distribution

| Travel Direction (to / from) | Percentage of Total Traffic Generation |
| :---: | :---: |
| North via Fuller Avenue | $0.8 \%$ |
| West via Sheffcote Street | $2.9 \%$ |
| South via Fuller Avenue | $45.6 \%$ |
| West via Robert Street East | $18.6 \%$ |
| North via Centennial Drive | $0.5 \%$ |
| South via Thompsons Road | $31.6 \%$ |
| TOTAL | $\mathbf{1 0 0 \%}$ |

It has been assumed all trips generated by the commercial block are to use the Commercial Access.
The distribution of traffic for the commercial component of this development is assumed to follow the distribution of the existing traffic volumes within the study area. Table 10 illustrates the calculation of the distribution of ingress and egress traffic for the commercial component of the proposed development.

Table 10 - Proposed Development Commercial Traffic Distribution

| Travel Direction (to / from) | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Ingress | Egress | Ingress | Egress |
| North via Fuller Avenue | $12 \%$ | $31 \%$ | $31 \%$ | $10 \%$ |
| West via Sheffcote Street | $4 \%$ | $1 \%$ | $2 \%$ | $4 \%$ |
| East via Pine Grove Road | $2 \%$ | $1 \%$ | $2 \%$ | $2 \%$ |
| South via Fuller Avenue | $40 \%$ | $32 \%$ | $31 \%$ | $36 \%$ |
| West via Robert Street East | $25 \%$ | $19 \%$ | $17 \%$ | $29 \%$ |
| North via Centennial Drive | $5 \%$ | $11 \%$ | $9 \%$ | $5 \%$ |
| South via Thompsons Road | $12 \%$ | $5 \%$ | $8 \%$ | $14 \%$ |
| TOTAL | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0} \%$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ |

Using the traffic distributions patterns noted above, the residential, commercial pass-by and commercial primary traffic assignment for the proposed development was calculated for the AM and PM peak hour and is illustrated in Figures 9, 10 and 11 respectively.

### 4.3 Total Horizon Year Traffic Volumes with the Proposed Development

For the total (2028) horizon year traffic volumes, the proposed development traffic was added to the background (2028) traffic volumes. The resulting total (2028) horizon year traffic volume for the AM and PM peak hour are illustrated in Figure 12.

Figure 9 - Proposed Development - Residential Traffic Assignment


Figure 10 - Proposed Development - Commercial Pass-by Traffic Assignment


Figure 11 - Proposed Development - Commercial Primary Traffic Assignment


Figure 12 - Total (2028) Traffic Volumes


## 5 Intersection Development <br> Operation <br> with <br> Proposed

### 5.1 Total (2028) Intersection Operation

The results of the LOS analysis under total (2028) traffic volumes during the AM and PM peak hour can be found below in Table 11. Existing intersection geometry and traffic control with the infrastructure improvements identified in Section 3.3 have been utilized for this scenario. Detailed output of the Synchro analysis can be found in Appendix H.

Table 11 - Total (2028) LOS

| Location <br> (N-S Street / E-W Street) | Weekday AM Peak Hour |  |  | Weekday PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C | Delay (s) | LOS | V/C | Delay (s) | LOS |
| Fuller Avenue / Pine Grove Road \& Sheffcote Street (unsignalized) | - | 3.4 | A | - | 3.4 | B |
| EB | 0.13 | 11.9 | B | 0.16 | 15.6 | C |
| WB | 0.32 | 25.8 | D | 0.29 | 30.7 | D |
| Thompsons Road \& Centennial Drive / Robert Street East (unsignalized) | - | 6.2 | A | - | 10.1 | C |
| NB | 0.38 | 18.9 | C | 0.39 | 19.5 | C |
| SB | 0.24 | 23.9 | C | 0.64 | 49.6 | E |
| Fuller Avenue / Robert Street East (signalized) | 0.47 | 15.2 | B | 0.52 | 15.4 | B |
| EBL | 0.61 | 35.5 | D | 0.58 | 34.9 | C |
| EBR | 0.17 | 29.9 | C | 0.16 | 30.0 | C |
| NBL | 0.41 | 5.6 | A | 0.48 | 6.1 | A |
| NBT | 0.26 | 5.4 | A | 0.19 | 4.9 | A |
| SBT | 0.33 | 12.9 | B | 0.43 | 14.0 | B |
| SBR | 0.10 | 10.8 | B | 0.27 | 12.2 | B |
| North Access / Pine Grove Road (unsignalized) | - | 3.4 | A | - | 1.7 | A |
| NB | 0.04 | 8.9 | A | 0.02 | 8.9 | A |
| Fuller Avenue / Commercial Access (unsignalized) | - | 0.2 | A | - | 0.6 | A |
| WB | 0.02 | 13.4 | B | 0.07 | 15.0 | B |
| Fuller Avenue / South Access (unsignalized) | - | 1.4 | A | - | 0.8 | A |
| WB | 0.18 | 16.4 | C | 0.13 | 18.0 | C |

The results of the LOS analysis indicate that all intersections are operating within the typical design limits noted in Section 3.1.

An analysis was completed for left turn movements at the unsignalized study area intersections, based on the criteria outlined in Appendix 9A of the MTO DS. Our analysis indicates that a left turn lane is warranted in the westbound direction at the Thompsons Road \& Centennial Drive / Robert Street East intersection and marginally warranted in the northbound direction at the Fuller Avenue / Pine Grove Road \& Sheffcote Street intersection (results are provided in Appendix D); however, reconstruction of this intersection is not recommended for this horizon year, based on our review of the traffic operations at this intersections, as illustrated in the Synchro analysis.

A review of the need for an auxiliary right turn lane at the unsignalized study area intersections was completed as part of our analysis. The results of the Synchro analysis indicate that there is excess capacity for all movements; consequently, additional auxiliary right turn lanes are not recommended.

The anticipated $95^{\text {th }}$ percentile queue length for all auxiliary turn lanes in the study area can be accommodated by the existing auxiliary lane storage lengths.

Based on the Ontario Traffic Manual Book 12 Signal Justification, traffic signals are not warranted at the unsignalized study area intersections (results are provided in Appendix E).

No additional infrastructure improvements are recommended within the study area.

### 5.2 Site Access

The North Access will operate efficiently as a full-movement access, with one-way stop control for the northbound movements. No lane improvements are recommended on Pine Grove Road at the North Access. A single northbound and southbound lane at the North Access driveway will provide the necessary capacity to service the proposed development.

The South Access will operate efficiently as a full-movement access, with one-way stop control for the westbound movements. No lane improvements are recommended on Fuller Avenue at the South Access. A single eastbound and westbound lane at the South Access driveway will provide the necessary capacity to service the proposed development.

The Commercial Access will operate efficiently as a full-movement access, with one-way stop control for the westbound movements. No lane improvements are recommended on Fuller Avenue at the Commercial Access. A single eastbound and westbound lane at the Commercial Access driveway will provide the necessary capacity to service the proposed development.

The proposed spacing between the North Access and the intersection of Pine Grove Road \& Sheffcote Street / Fuller Avenue (measured edge to edge of driveways) and the North Access and the intersection of Pine Grove Road / Margaret Crescent (measured edge to edge of driveways) is in excess of the suggested minimum corner clearance requirements for a driveway as identified in the Transportation Association of Canada Design Guide for Canadian Roads (2017) [TAC Guidelines] Figure 8.8.2 (Suggested Minimum Corner Clearances to Accesses or Public Lanes at Major Intersections) - 15 metres for unsignalized condition.

The proposed spacing between the South Access and the intersection of Pine Grove Road \& Sheffcote Street / Fuller Avenue (measured edge to edge of driveways) and the South Access and the intersection of Cambridge Street / Fuller Avenue (measured edge to edge of driveways) is in excess of the suggested minimum corner clearance requirements for a driveway as identified in the TAC Guidelines - Figure 8.8.2 (Suggested Minimum Corner Clearances to Accesses or Public Lanes at Major Intersections) - 35 metres for unsignalized condition.

The intersection spacing for the Commercial Access has not been analysed in this study as the specifics of the proposed development commercial block access driveways are currently unknown.

### 5.3 Sight Distance Review

A review of the available sight distance for the proposed site access driveways was completed as part of this analysis.

The sight distance east and west of the North Access is greater than the minimum stopping sight distance requirements as identified in the TAC Guidelines for a design speed of $60 \mathrm{~km} / \mathrm{h}$ ( 85 metres). It is noted that the Pine Grove Road \& Sheffcote Street / Fuller Avenue intersection is located approximately 85 metres west of the North Access; however, there are no concerns with the sight distance since vehicles from Fuller Avenue turning onto Pine Grove Road will be travelling at speeds much lower than $60 \mathrm{~km} / \mathrm{h}$.

The sight distance north and south of the South Access is greater than the minimum stopping sight distance requirements as identified in the TAC Guidelines for a design speed of $70 \mathrm{~km} / \mathrm{h}$ ( 105 metres).

Consequently, there are no issues with the sight distance for the proposed site access driveways.
The sight distance available for the Commercial Access has not been analysed in this study as the specifics of the proposed development commercial block access driveways are currently unknown.

## 6 Summary

Tonking Management Inc. retained JD Engineering to prepare this traffic impact study in support of the proposed mixed-use development municipally known as 1145 Fuller Avenue proposed in the Town of Penetanguishene [Town], County of Simcoe [County]. The proposed Site Plan is shown in Appendix A. This chapter summarizes the conclusions and recommendations from the study.

The proposed residential development includes a 0.56 acres commercial block, 102 residential single detached units, 86 residential townhouse units and a 0.56 acre residential multi-density block. The specifics of the residential multi-density lands are currently unknown; however, based on discussions with the developer, it is anticipated there will be a maximum of 20 residential units.

1. The proposed development is expected to generate a total of 140 AM peak hour trips and 204 PM peak hour trips.
2. Detailed turning movement counts were completed for all existing intersections on Tuesday, November $6{ }^{\text {th }}, 2018$.
3. An intersection operation analysis was completed at the study area intersections, using the existing (2018) and background (2028) traffic volumes, with the adjacent development traffic and without the proposed development traffic. This enabled a review of existing and future traffic deficiencies that would be present without the influence of the proposed development. The following transportation infrastructure improvements are recommended:

## Fuller Avenue / Robert Street East

Background (2028) Traffic Volumes

- Signalization of intersection;
- Northbound left turn auxiliary lane;
- (45 metre storage length and 55 metre taper length)
- Southbound right turn auxiliary lane;
- ( 30 metre storage length and 60 metre taper length)
- Eastbound right turn auxiliary lane.
- (30 metre storage length and 30 metre taper length)

4. An estimate of the amount of traffic that would be generated by the proposed development was prepared and assigned to the study area streets and intersections.
5. An intersection operation analysis was completed under total (2028) traffic volumes with the proposed development operational at the study area intersections. No additional infrastructure improvements are recommended.
6. The proposed South Access and Commercial Access driveways will operate efficiently as full movement access driveways with one-way stop control for westbound traffic. The proposed North Access driveway will operate efficiently as a full movement access driveway with one-way stop control for northbound traffic. A single lane for ingress and egress movements at the South Access, Commercial Access and North Access will provide the necessary capacity to convey the traffic volume generated by the proposed development.
7. The sight distance available for the proposed South Access and North Access meets the minimum stopping sight distance requirements. The sight distance available for the Commercial Access has not been analysed in this study as the specifics of the proposed development commercial block access driveways are currently unknown.
8. In summary, the proposed development will not cause any operational issues and will not add a notable delay or congestion to the local roadway network.

## Appendix A Site Plan



## Appendix B Traffic Count Data



## Accu-Traffic Inc.



Comments

## Accu-Traffic Inc.

## Total Count Diagram



Comments

Accu-Traffic Inc
Traffic Monitoring \& Data Analysis


## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300001


## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300001


## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300001

| Interval Time | Passenger Cars - South Approach |  |  |  |  |  | Trucks - South Approach |  |  |  |  |  | Heavys - South Approach |  |  |  |  |  | Pedestrians |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | South Cross |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 2 | 2 | 31 | 31 | 0 | 0 | 0 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30:00 | 3 | 1 | 87 | 56 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45:00 | 3 | 0 | 155 | 68 | 1 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 |
| 8:00:00 | 4 | 1 | 279 | 124 | 2 | 1 | 0 | 0 | 5 | 1 | 0 | 0 | 1 | 1 | 2 | 1 | 0 | 0 | 0 | 0 |
| 8:15:00 | 5 | 1 | 350 | 71 | 6 | 4 | 0 | 0 | 5 | 0 | 0 | 0 | 1 | 0 | 3 | 1 | 0 | 0 | 0 | 0 |
| 8:30:00 | 10 | 5 | 403 | 53 | 8 | 2 | 0 | 0 | 6 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 1 | 1 | 0 | 0 |
| 8:45:00 | 12 | 2 | 424 | 21 | 15 | 7 | 0 | 0 | 7 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 1 | 0 | 0 | 0 |
| 9:00:00 | 16 | 4 | 454 | 30 | 17 | 2 | 0 | 0 | 8 | 1 | 0 | 0 | 1 | 0 | 4 | 1 | 2 | 1 | 0 | 0 |
| 9:15:00 | 16 | 0 | 454 | 0 | 17 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 2 | 0 | 0 | 0 |
| 16:00:00 | 16 | 0 | 454 | 0 | 17 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 2 | 0 | 0 | 0 |
| 16:15:00 | 24 | 8 | 467 | 13 | 21 | 4 | 0 | 0 | 8 | 0 | 0 | 0 | 1 | 0 | 5 | 1 | 2 | 0 | 0 | 0 |
| 16:30:00 | 33 | 9 | 490 | 23 | 26 | 5 | 0 | 0 | 8 | 0 | 0 | 0 | 1 | 0 | 5 | 0 | 3 | 1 | 0 | 0 |
| 16:45:00 | 45 | 12 | 521 | 31 | 29 | 3 | 0 | 0 | 8 | 0 | 0 | 0 | 1 | 0 | 5 | 0 | 3 | 0 | 0 | 0 |
| 17:00:00 | 51 | 6 | 568 | 47 | 34 | 5 | 0 | 0 | 8 | 0 | 0 | 0 | 1 | 0 | 5 | 0 | 3 | 0 | 0 | 0 |
| 17:15:00 | 57 | 6 | 594 | 26 | 39 | 5 | 0 | 0 | 8 | 0 | 0 | 0 | 1 | 0 | 5 | 0 | 3 | 0 | 0 | 0 |
| 17:30:00 | 68 | 11 | 637 | 43 | 44 | 5 | 0 | 0 | 9 | 1 | 0 | 0 | 1 | 0 | 6 | 1 | 3 | 0 | 0 | 0 |
| 17:45:00 | 72 | 4 | 658 | 21 | 45 | 1 | 0 | 0 | 9 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 0 | 0 |
| 18:00:00 | 80 | 8 | 686 | 28 | 49 | 4 | 0 | 0 | 10 | 1 | 0 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 1 | 1 |
| 18:15:00 | 86 | 6 | 720 | 34 | 50 | 1 | 0 | 0 | 10 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 1 | 0 |
| 18:30:00 | 90 | 4 | 763 | 43 | 53 | 3 | 0 | 0 | 10 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 1 | 0 |
| 18:45:00 | 96 | 6 | 795 | 32 | 54 | 1 | 0 | 0 | 10 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 1 | 0 |
| 19:00:00 | 104 | 8 | 822 | 27 | 56 | 2 | 0 | 0 | 10 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 1 | 0 |
| 19:15:00 | 104 | 0 | 822 | 0 | 56 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 1 | 0 |
| 19:15:15 | 104 | 0 | 822 | 0 | 56 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 1 | 0 |
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## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300001

| Interval Time | Passenger Cars - West Approach |  |  |  |  |  | Trucks - West Approach |  |  |  |  |  | Heavys - West Approach |  |  |  |  |  | Pedestrians |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | West Cross |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 0 | 0 | 0 | 0 | 9 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30:00 | 1 | 1 | 0 | 0 | 17 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45:00 | 1 | 0 | 0 | 0 | 26 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00:00 | 3 | 2 | 0 | 0 | 34 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15:00 | 5 | 2 | 0 | 0 | 40 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| 8:30:00 | 5 | 0 | 0 | 0 | 51 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 1 | 1 | 0 | 0 | 0 |
| 8:45:00 | 6 | 1 | 1 | 1 | 61 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 1 | 0 | 0 |
| 9:00:00 | 7 | 1 | 1 | 0 | 67 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 9:15:00 | 7 | 0 | 1 | 0 | 67 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 16:00:00 | 7 | 0 | 1 | 0 | 67 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 16:15:00 | 7 | 0 | 1 | 0 | 74 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 16:30:00 | 8 | 1 | 1 | 0 | 76 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 16:45:00 | 9 | 1 | 1 | 0 | 78 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 17:00:00 | 9 | 0 | 1 | 0 | 85 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 17:15:00 | 9 | 0 | 1 | 0 | 91 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 17:30:00 | 9 | 0 | 1 | 0 | 98 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 17:45:00 | 9 | 0 | 1 | 0 | 101 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 18:00:00 | 9 | 0 | 1 | 0 | 105 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 |
| 18:15:00 | 9 | 0 | 1 | 0 | 111 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 1 | 1 |
| 18:30:00 | 9 | 0 | 1 | 0 | 113 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 1 | 0 |
| 18:45:00 | 9 | 0 | 2 | 1 | 118 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 1 | 0 |
| 19:00:00 | 9 | 0 | 2 | 0 | 119 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 1 | 0 |
| 19:15:00 | 9 | 0 | 2 | 0 | 119 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 1 | 0 |
| 19:15:15 | 9 | 0 | 2 | 0 | 119 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 1 | 0 |
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## Accu-Traffic Inc.



Comments

## Accu-Traffic Inc.



Comments

## Accu-Traffic Inc.

## Total Count Diagram



Comments

Accu-Traffic Inc
Traffic Monitoring \& Data Analysis


## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300002

| Interval Time | Passenger Cars - North Approach |  |  |  |  |  | Trucks - North Approach |  |  |  |  |  | Heavys - North Approach |  |  |  |  |  | Pedestrians |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | North Cross |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 0 | 0 | 42 | 42 | 14 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30:00 | 0 | 0 | 83 | 41 | 33 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45:00 | 0 | 0 | 115 | 32 | 45 | 12 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00:00 | 0 | 0 | 153 | 38 | 62 | 17 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 |
| 8:15:00 | 0 | 0 | 185 | 32 | 73 | 11 | 0 | 0 | 3 | 1 | 1 | 0 | 0 | 0 | 4 | 3 | 1 | 1 | 0 | 0 |
| 8:30:00 | 0 | 0 | 229 | 44 | 85 | 12 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 4 | 0 | 2 | 1 | 0 | 0 |
| 8:45:00 | 0 | 0 | 265 | 36 | 100 | 15 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 5 | 1 | 2 | 0 | 0 | 0 |
| 9:00:00 | 0 | 0 | 297 | 32 | 114 | 14 | 0 | 0 | 5 | 2 | 1 | 0 | 0 | 0 | 5 | 0 | 4 | 2 | 0 | 0 |
| 9:15:00 | 0 | 0 | 297 | 0 | 114 | 0 | 0 | 0 | 5 | 0 | 1 | 0 | 0 | 0 | 5 | 0 | 4 | 0 | 0 | 0 |
| 16:00:00 | 0 | 0 | 297 | 0 | 114 | 0 | 0 | 0 | 5 | 0 | 1 | 0 | 0 | 0 | 5 | 0 | 4 | 0 | 0 | 0 |
| 16:15:00 | 0 | 0 | 398 | 101 | 196 | 82 | 0 | 0 | 7 | 2 | 1 | 0 | 0 | 0 | 5 | 0 | 5 | 1 | 0 | 0 |
| 16:30:00 | 0 | 0 | 444 | 46 | 240 | 44 | 0 | 0 | 7 | 0 | 1 | 0 | 0 | 0 | 5 | 0 | 6 | 1 | 0 | 0 |
| 16:45:00 | 0 | 0 | 498 | 54 | 283 | 43 | 0 | 0 | 8 | 1 | 2 | 1 | 0 | 0 | 5 | 0 | 7 | 1 | 0 | 0 |
| 17:00:00 | 0 | 0 | 539 | 41 | 307 | 24 | 0 | 0 | 8 | 0 | 2 | 0 | 0 | 0 | 7 | 2 | 8 | 1 | 0 | 0 |
| 17:15:00 | 0 | 0 | 575 | 36 | 327 | 20 | 0 | 0 | 9 | 1 | 2 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 17:30:00 | 0 | 0 | 595 | 20 | 342 | 15 | 0 | 0 | 9 | 0 | 2 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 17:45:00 | 0 | 0 | 619 | 24 | 356 | 14 | 0 | 0 | 9 | 0 | 2 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 18:00:00 | 0 | 0 | 650 | 31 | 375 | 19 | 0 | 0 | 9 | 0 | 4 | 2 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 18:15:00 | 0 | 0 | 664 | 14 | 386 | 11 | 0 | 0 | 12 | 3 | 4 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 18:30:00 | 0 | 0 | 685 | 21 | 400 | 14 | 0 | 0 | 12 | 0 | 4 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 18:45:00 | 0 | 0 | 722 | 37 | 427 | 27 | 0 | 0 | 12 | 0 | 4 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 19:00:00 | 0 | 0 | 760 | 38 | 457 | 30 | 0 | 0 | 12 | 0 | 4 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 19:15:00 | 0 | 0 | 760 | 0 | 457 | 0 | 0 | 0 | 12 | 0 | 4 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
| 19:15:15 | 0 | 0 | 760 | 0 | 457 | 0 | 0 | 0 | 12 | 0 | 4 | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 0 | 0 |
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## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300002


## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300002

| Interval Time | Passenger Cars - South Approach |  |  |  |  |  | Trucks - South Approach |  |  |  |  |  | Heavys - South Approach |  |  |  |  |  | Pedestrians |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | South Cross |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 22 | 22 | 24 | 24 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 |
| 7:30:00 | 36 | 14 | 58 | 34 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 |
| 7:45:00 | 62 | 26 | 105 | 47 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 1 | 3 | 1 | 0 | 0 | 0 | 0 |
| 8:00:00 | 100 | 38 | 204 | 99 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 5 | 3 | 4 | 1 | 0 | 0 | 0 | 0 |
| 8:15:00 | 143 | 43 | 240 | 36 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 8 | 3 | 4 | 0 | 0 | 0 | 0 | 0 |
| 8:30:00 | 186 | 43 | 272 | 32 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 8 | 0 | 5 | 1 | 0 | 0 | 0 | 0 |
| 8:45:00 | 243 | 57 | 294 | 22 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 8 | 0 | 6 | 1 | 0 | 0 | 0 | 0 |
| 9:00:00 | 291 | 48 | 324 | 30 | 0 | 0 | 2 | 2 | 4 | 0 | 0 | 0 | 8 | 0 | 8 | 2 | 0 | 0 | 0 | 0 |
| 9:15:00 | 291 | 0 | 324 | 0 | 0 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 |
| 16:00:00 | 291 | 0 | 324 | 0 | 0 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 |
| 16:15:00 | 335 | 44 | 347 | 23 | 0 | 0 | 2 | 0 | 5 | 1 | 0 | 0 | 10 | 2 | 9 | 1 | 0 | 0 | 0 | 0 |
| 16:30:00 | 403 | 68 | 387 | 40 | 0 | 0 | 2 | 0 | 5 | 0 | 0 | 0 | 11 | 1 | 9 | 0 | 0 | 0 | 0 | 0 |
| 16:45:00 | 464 | 61 | 420 | 33 | 0 | 0 | 2 | 0 | 5 | 0 | 0 | 0 | 12 | 1 | 9 | 0 | 0 | 0 | 0 | 0 |
| 17:00:00 | 503 | 39 | 449 | 29 | 0 | 0 | 2 | 0 | 6 | 1 | 0 | 0 | 12 | 0 | 9 | 0 | 0 | 0 | 0 | 0 |
| 17:15:00 | 547 | 44 | 474 | 25 | 0 | 0 | 3 | 1 | 6 | 0 | 0 | 0 | 13 | 1 | 9 | 0 | 0 | 0 | 0 | 0 |
| 17:30:00 | 589 | 42 | 511 | 37 | 0 | 0 | 3 | 0 | 7 | 1 | 0 | 0 | 13 | 0 | 10 | 1 | 0 | 0 | 0 | 0 |
| 17:45:00 | 635 | 46 | 530 | 19 | 0 | 0 | 3 | 0 | 8 | 1 | 0 | 0 | 13 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 18:00:00 | 660 | 25 | 549 | 19 | 0 | 0 | 3 | 0 | 8 | 0 | 0 | 0 | 13 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 18:15:00 | 680 | 20 | 576 | 27 | 0 | 0 | 4 | 1 | 8 | 0 | 0 | 0 | 13 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 18:30:00 | 700 | 20 | 613 | 37 | 0 | 0 | 4 | 0 | 8 | 0 | 0 | 0 | 13 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 18:45:00 | 720 | 20 | 636 | 23 | 0 | 0 | 4 | 0 | 8 | 0 | 0 | 0 | 13 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 19:00:00 | 738 | 18 | 658 | 22 | 0 | 0 | 4 | 0 | 8 | 0 | 0 | 0 | 13 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 19:15:00 | 738 | 0 | 658 | 0 | 0 | 0 | 4 | 0 | 8 | 0 | 0 | 0 | 13 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 19:15:15 | 738 | 0 | 658 | 0 | 0 | 0 | 4 | 0 | 8 | 0 | 0 | 0 | 13 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
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## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300002




## Accu-Traffic Inc.

## Total Count Diagram



Comments

Accu-Traffic Inc
Traffic Monitoring \& Data Analysis


## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300003


## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300003


## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300003

| Interval Time | Passenger Cars - South Approach |  |  |  |  |  | Trucks - South Approach |  |  |  |  |  | Heavys - South Approach |  |  |  |  |  | Pedestrians |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | South Cross |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 0 | 0 | 3 | 3 | 12 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 |
| 7:30:00 | 1 | 1 | 5 | 2 | 21 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 |
| 7:45:00 | 1 | 0 | 13 | 8 | 37 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 |
| 8:00:00 | 2 | 1 | 31 | 18 | 57 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 2 | 2 |
| 8:15:00 | 2 | 0 | 47 | 16 | 68 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 3 | 1 | 1 | 2 | 0 |
| 8:30:00 | 2 | 0 | 52 | 5 | 82 | 14 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 9 | 2 | 2 | 1 | 2 | 0 |
| 8:45:00 | 4 | 2 | 56 | 4 | 92 | 10 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 10 | 1 | 2 | 0 | 2 | 0 |
| 9:00:00 | 4 | 0 | 63 | 7 | 101 | 9 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 12 | 2 | 2 | 0 | 2 | 0 |
| 9:15:00 | 4 | 0 | 63 | 0 | 101 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 2 | 0 | 2 | 0 |
| 16:00:00 | 4 | 0 | 63 | 0 | 101 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 2 | 0 | 2 | 0 |
| 16:15:00 | 5 | 1 | 68 | 5 | 109 | 8 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 14 | 2 | 2 | 0 | 2 | 0 |
| 16:30:00 | 6 | 1 | 76 | 8 | 124 | 15 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 2 | 0 | 2 | 0 |
| 16:45:00 | 7 | 1 | 81 | 5 | 144 | 20 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 2 | 0 | 2 | 0 |
| 17:00:00 | 9 | 2 | 86 | 5 | 160 | 16 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 15 | 1 | 2 | 0 | 2 | 0 |
| 17:15:00 | 10 | 1 | 91 | 5 | 168 | 8 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 2 | 0 | 2 | 0 |
| 17:30:00 | 12 | 2 | 98 | 7 | 179 | 11 | 0 | 0 | 2 | 0 | 1 | 1 | 0 | 0 | 16 | 1 | 2 | 0 | 2 | 0 |
| 17:45:00 | 13 | 1 | 103 | 5 | 185 | 6 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 17 | 1 | 2 | 0 | 2 | 0 |
| 18:00:00 | 14 | 1 | 105 | 2 | 196 | 11 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 17 | 0 | 2 | 0 | 2 | 0 |
| 18:15:00 | 16 | 2 | 108 | 3 | 212 | 16 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 17 | 0 | 2 | 0 | 2 | 0 |
| 18:30:00 | 19 | 3 | 108 | 0 | 223 | 11 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 17 | 0 | 2 | 0 | 2 | 0 |
| 18:45:00 | 20 | 1 | 110 | 2 | 235 | 12 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 17 | 0 | 3 | 1 | 2 | 0 |
| 19:00:00 | 22 | 2 | 112 | 2 | 243 | 8 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 17 | 0 | 3 | 0 | 2 | 0 |
| 19:15:00 | 22 | 0 | 112 | 0 | 243 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 17 | 0 | 3 | 0 | 2 | 0 |
| 19:15:15 | 22 | 0 | 112 | 0 | 243 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 17 | 0 | 3 | 0 | 2 | 0 |
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## Accu-Traffic Inc.

Count Date: 6-Nov-18 Site \#: 1814300003

| Interval Time | Passenger Cars - West Approach |  |  |  |  |  | Trucks - West Approach |  |  |  |  |  | Heavys - West Approach |  |  |  |  |  | Pedestrians |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | West Cross |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 4 | 4 | 18 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| 7:30:00 | 12 | 8 | 59 | 41 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 0 | 0 |
| 7:45:00 | 21 | 9 | 115 | 56 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 |
| 8:00:00 | 34 | 13 | 164 | 49 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 1 | 0 | 0 | 0 |
| 8:15:00 | 48 | 14 | 202 | 38 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 4 | 1 | 1 | 0 | 0 | 0 |
| 8:30:00 | 55 | 7 | 254 | 52 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 6 | 2 | 1 | 0 | 0 | 0 |
| 8:45:00 | 58 | 3 | 308 | 54 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 6 | 0 | 1 | 0 | 0 | 0 |
| 9:00:00 | 60 | 2 | 364 | 56 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 10 | 4 | 1 | 0 | 0 | 0 |
| 9:15:00 | 60 | 0 | 364 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 10 | 0 | 1 | 0 | 0 | 0 |
| 16:00:00 | 60 | 0 | 364 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 10 | 0 | 1 | 0 | 0 | 0 |
| 16:15:00 | 64 | 4 | 397 | 33 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 11 | 1 | 1 | 0 | 0 | 0 |
| 16:30:00 | 69 | 5 | 434 | 37 | 7 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 16:45:00 | 71 | 2 | 480 | 46 | 11 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 17:00:00 | 77 | 6 | 519 | 39 | 14 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 11 | 0 | 1 | 0 | 0 | 0 |
| 17:15:00 | 82 | 5 | 558 | 39 | 17 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 17:30:00 | 84 | 2 | 586 | 28 | 17 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 17:45:00 | 86 | 2 | 612 | 26 | 17 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 11 | 0 | 1 | 0 | 0 | 0 |
| 18:00:00 | 89 | 3 | 652 | 40 | 17 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 18:15:00 | 91 | 2 | 685 | 33 | 18 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 18:30:00 | 94 | 3 | 704 | 19 | 21 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 18:45:00 | 96 | 2 | 721 | 17 | 21 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 19:00:00 | 97 | 1 | 738 | 17 | 22 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 19:15:00 | 97 | 0 | 738 | 0 | 22 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
| 19:15:15 | 97 | 0 | 738 | 0 | 22 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 1 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Appendix C Synchro Analysis Output Existing Traffic Volumes

|  | $\rangle$ |  |  | 7 | $\downarrow$ |  | 4 | $\dagger$ | + |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | \$ |  |  | ¢ |  |  | $\$$ |  |
| Traffic Volume (veh/h) | 6 | 1 | 35 | 18 | 2 | 1 | 8 | 321 | 9 | 1 | 110 | 1 |
| Future Volume (Veh/h) | 6 | 1 | 35 | 18 | 2 | 1 | 8 | 321 | 9 | 1 | 110 | 1 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 |
| Hourly flow rate (vph) | 8 | 1 | 49 | 25 | 3 | 1 | 11 | 446 | 13 | 1 | 153 | 1 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 632 | 636 | 154 | 680 | 630 | 452 | 154 |  |  | 459 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 632 | 636 | 154 | 680 | 630 | 452 | 154 |  |  | 459 |  |  |
| tC, single (s) | 7.4 | 7.5 | 6.2 | 7.1 | 7.5 | 7.2 | 4.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.8 | 4.9 | 3.3 | 3.5 | 4.9 | 4.2 | 2.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 98 | 100 | 94 | 93 | 99 | 100 | 99 |  |  | 100 |  |  |
| cM capacity (veh/h) | 346 | 289 | 890 | 344 | 292 | 446 | 1362 |  |  | 1113 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total | 58 | 29 | 470 | 155 |  |  |  |  |  |  |  |  |
| Volume Left | 8 | 25 | 11 | 1 |  |  |  |  |  |  |  |  |
| Volume Right | 49 | 1 | 13 | 1 |  |  |  |  |  |  |  |  |
| cSH | 711 | 341 | 1362 | 1113 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.08 | 0.09 | 0.01 | 0.00 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 2.1 | 2.2 | 0.2 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 10.5 | 16.5 | 0.3 | 0.1 |  |  |  |  |  |  |  |  |
| Lane LOS | B | C | A | A |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 10.5 | 16.5 | 0.3 | 0.1 |  |  |  |  |  |  |  |  |
| Approach LOS | B | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.7 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 34.1\% | ICU Level of Service |  |  |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |







## Appendix D - <br> MTO Left Turn Warrant Analysis




Exhibit 9A-12 Background (2028) - northbound PM Peak Hour (critical scenario)


TRAFFIC SIGNALS MAY BE WARRANTED IN RURAL AREAS OR URBAN AREAS WITH RESTRICTED FLOW

TRAFFIC SIGNALS MAY BE WARRANTED IN "FREE FLOW" URBAN AREAS


Exhibit 9A-12 Total (2028) - northbound PM Peak Hour (critical scenario)


TRAFFIC SIGNALS MAY BE WARRANTED IN RURAL AREAS OR URBAN AREAS WITH RESTRICTED FLOW

TRAFFIC SIGNALS MAY BE WARRANTED IN "FREE FLOW" URBAN AREAS


Exhibit 9A-13



Robert Street / Fuller Street
Existing (2018) - northbound
AM Peak Hour (critical scenario)


Exhibit 9A-12
Existing (2018) - westbound PM Peak Hour (critical scenario)


TRAFFIC SIGNALS MAY BE WARRANTED IN RURAL AREAS OR URBAN AREAS WITH RESTRICTED FLOW

TRAFFIC SIGNALS MAY BE WARRANTED IN "FREE FLOW" URBAN AREAS


Exhibit 9A－12

－ーー一 TRAFFIC SIGNALS MAY BE WARRANTED IN RURAL
AREAS OR URBAN AREAS WITH RESTRICTED FLOW
TRAFFIC SIGNALS MAY BE WARRANTED IN
＂FREE FLOW＂URBAN AREAS
Robert St／Thompsons Rd \＆Centennial Dr Background（2028）－westbound PM Peak Hour（critical scenario）


Exhibit 9A-12


TRAFFIC SIGNALS MAY BE WARRANTED IN RURAL
AREAS OR URBAN AREAS WITH RESTRICTED FLOW
TRAFFIC SIGNALS MAY BE WARRANTED IN
"FREE FLOW" URBAN AREAS
Robert St / Thompsons Rd \& Centennial Dr
Total (2028) - westbound
PM Peak Hour (critical scenario)


Exhibit 9A－11 Total（2028）－eastbound
AM Peak Hour（critical scenario）


ーーーーー TRAFFIC SIGNALS MAY BE WARRANTED IN RURAL AREAS OR URBAN AREAS WITH RESTRICTED FLOW

TRAFFIC SIGNALS MAY BE WARRANTED IN ＂FREE FLOW＂URBAN AREAS


## Appendix E- <br> OTM Signal Justification Sheets

## Justification No. 7-2028 Total Traffic (Critical Case)

Pine Grove Road / North Access

| Justification | Description |  | Compliance |  |  | Signal Warrant | Underground Provisions Warrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sectional |  | Entire \% |  |  |
|  |  | Rest. Flow | Numerical | \% |  |  |  |
| 1. Minimum Vehicluar Volume | A. Vehicle volume, all aproaches (average hour) | 720 | 44 | 6\% | 3\% | NO | NO |
|  | B. Vehicle volume, along minor streets (average hour) | 255 | 12 | 5\% |  | NO | NO |
| 2. Delay to cross traffic | A. Vehicle volume, major street (average hour) | 720 | 22 | 3\% | 2\% | NO | NO |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 75 | 12 | 16\% |  | NO | NO |

## Justification No. 7-2028 Total Traffic (Critical Case)

South Access / Fuller Avenue

| Justification | Description |  | Compliance |  |  | Signal Warrant | Underground Provisions Warrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sectional |  | Entire \% |  |  |
|  |  | Rest. Flow | Numerical | \% |  |  |  |
| 1. Minimum Vehicluar Volume | A. Vehicle volume, all aproaches (average hour) | 720 | 410 | 57\% | 7\% | NO | NO |
|  | B. Vehicle volume, along minor streets (average hour) | 255 | 26 | 10\% |  | NO | NO |
| 2. Delay to cross traffic | A. Vehicle volume, major street (average hour) | 720 | 363 | 50\% | 23\% | NO | NO |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 75 | 26 | 34\% |  | NO | NO |

## Justification No. 7-2028 Total Traffic (Critical Case)

Commercial Access / Fuller Avenue

| Justification | Description |  | Compliance |  |  | Signal Warrant | Underground Provisions Warrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sectional |  | Entire \% |  |  |
|  |  | Rest. Flow | Numerical | \% |  |  |  |
| 1. Minimum Vehicluar Volume | A. Vehicle volume, all aproaches (average hour) | 720 | 369 | 51\% | 2\% | NO | NO |
|  | B. Vehicle volume, along minor streets (average hour) | 255 | 8 | 3\% |  | NO | NO |
| 2. Delay to cross traffic | A. Vehicle volume, major street (average hour) | 720 | 355 | 49\% | 5\% | NO | NO |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 75 | 6 | 8\% |  | NO | NO |

## Justification No. 7-2028 Total Traffic (Critical Case)

Robert Street / Fuller Avenue

| Justification | Description |  | Compliance |  |  | Signal Warrant | Underground Provisions Warrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sectional |  | Entire \% |  |  |
|  |  | Rest. Flow | Numerical | \% |  |  |  |
| 1. Minimum Vehicluar Volume | A. Vehicle volume, all aproaches (average hour) | 720 | 669 | 93\% | 58\% | NO | NO |
|  | B. Vehicle volume, along minor streets (average hour) | 255 | 179 | 70\% |  | NO | NO |
| 2. Delay to cross traffic | A. Vehicle volume, major street (average hour) | 720 | 387 | 54\% | 45\% | NO | NO |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 75 | 72 | 96\% |  | NO | NO |

## Justification No. 7-2028 Total Traffic (Critical Case)

Robert Street / Thomspons Road \& Centennial Dr

| Justification | Description |  | Compliance |  |  | Signal Warrant | Underground Provisions Warrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sectional |  | Entire \% |  |  |
|  |  | Rest. Flow | Numerical | \% |  |  |  |
| 1. Minimum Vehicluar Volume | A. Vehicle volume, all aproaches (average hour) | 720 | 486 | 67\% | 56\% | NO | NO |
|  | B. Vehicle volume, along minor streets (average hour) | 170 | 118 | 69\% |  | NO | NO |
|  | A. Vehicle volume, major street (average hour) | 720 | 350 | 49\% | 41\% | NO | NO |
| 2. Delay to cross traffic | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 75 | 37 | 50\% |  | NO | NO |

## Justification No. 7-2028 Total Traffic (Critical Case)

Sheffcote Road \& Pine Grove Road / Fuller Avenue

| Justification | Description |  | Compliance |  |  | Signal <br> Warrant | Underground Provisions Warrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sectional |  | Entire \% |  |  |
|  |  | Rest. Flow | Numerical | \% |  |  |  |
| 1. Minimum Vehicluar Volume | A. Vehicle volume, all aproaches (average hour) | 720 | 369 | 51\% | 25\% | NO | NO |
|  | B. Vehicle volume, along minor streets (average hour) | 170 | 51 | 30\% |  | NO | NO |
|  | A. Vehicle volume, major street (average hour) | 720 | 298 | 41\% | 29\% | NO | NO |
| 2. Delay to cross traffic | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 75 | 27 | 35\% |  | NO | NO |

## Appendix F Synchro Analysis Output Background Traffic Volumes

|  | 4 | $\rightarrow$ | $\cdots$ | 7 | $4$ | 4 | 4 | $\dagger$ | \% | ( | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | * |  |  | \$ |  |  | \$ |  |
| Traffic Volume (veh/h) | 8 | 1 | 47 | 23 | 2 | 1 | 12 | 393 | 11 | 1 | 136 | 2 |
| Future Volume (Veh/h) | 8 | 1 | 47 | 23 | 2 | 1 | 12 | 393 | 11 | 1 | 136 | 2 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 |
| Hourly flow rate (vph) | 11 | 1 | 65 | 32 | 3 | 1 | 17 | 546 | 15 | 1 | 189 | 3 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type None None |  |  |  |  |  |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 782 | 788 | 190 | 846 | 782 | 554 | 192 |  |  | 561 |  |  |
| vC 1 , stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC 2 , stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 782 | 788 | 190 | 846 | 782 | 554 | 192 |  |  | 561 |  |  |
| tC , single (s) | 7.4 | 7.5 | 6.2 | 7.1 | 7.5 | 7.2 | 4.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.8 | 4.9 | 3.3 | 3.5 | 4.9 | 4.2 | 2.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 96 | 100 | 92 | 88 | 99 | 100 | 99 |  |  | 100 |  |  |
| cM capacity (veh/h) | 271 | 229 | 849 | 259 | 231 | 385 | 1318 |  |  | 1020 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total | 77 | 36 | 578 | 193 |  |  |  |  |  |  |  |  |
| Volume Left | 11 | 32 | 17 | 1 |  |  |  |  |  |  |  |  |
| Volume Right | 65 | 1 | 15 | 3 |  |  |  |  |  |  |  |  |
|  | 633 | 259 | 1318 | 1020 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.12 | 0.14 | 0.01 | 0.00 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 3.3 | 3.8 | 0.3 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s)Lane LOS | 11.5 | 21.1 | 0.4 | 0.1 |  |  |  |  |  |  |  |  |
|  | B | C | A | A |  |  |  |  |  |  |  |  |
| Lane LOS | 11.5 | 21.1 | 0.4 | 0.1 |  |  |  |  |  |  |  |  |
| Approach LOS | B | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 42.2\% |  | Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |




|  | 4 | $\rightarrow$ | $\checkmark$ | 7 | $\downarrow$ | 4 | 4 | $\dagger$ | \% |  | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | $\ddagger$ |  |  | \$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 6 | 0 | 38 | 16 | 2 | 5 | 56 | 140 | 22 | 1 | 436 | 12 |
| Future Volume (Veh/h) | 6 | 0 | 38 | 16 | 2 | 5 | 56 | 140 | 22 | 1 | 436 | 12 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| Hourly flow rate (vph) | 8 | 0 | 51 | 22 | 3 | 7 | 76 | 189 | 30 | 1 | 589 | 16 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type None None |  |  |  |  |  |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 964 | 970 | 597 | 1006 | 963 | 204 | 605 |  |  | 219 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked voltC , single (s) | 964 | 970 | 597 | 1006 | 963 | 204 | 605 |  |  | 219 |  |  |
|  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{tF}(\mathrm{s})$ | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 96 | 100 | 90 | 88 | 99 | 99 | 92 |  |  | 100 |  |  |
| cM capacity (veh/h) | 219 | 235 | 507 | 187 | 237 | 842 | 983 |  |  | 1362 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total | 59 | 32 | 295 | 606 |  |  |  |  |  |  |  |  |
| Volume Left | 8 | 22 | 76 | 1 |  |  |  |  |  |  |  |  |
| Volume Right | 51 | 7 | 30 | 16 |  |  |  |  |  |  |  |  |
|  | 430 | 231 | 983 | 1362 |  |  |  |  |  |  |  |  |
| CSH | 0.14 | 0.14 | 0.08 | 0.00 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 3.8 | 3.8 | 2.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 14.7 | 23.0 | 2.9 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | B | C | A | A |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 14.7 | 23.0 | 2.9 | 0.0 |  |  |  |  |  |  |  |  |
| Approach LOS | B | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 50.2\% |  | Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |




|  | 4 |  | 4 |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 | \% | 4 | 4 | T |
| Traffic Volume (vph) | 125 | 206 | 236 | 239 | 193 | 74 |
| Future Volume (vph) | 125 | 206 | 236 | 239 | 193 | 74 |
| Lane Group Flow (vph) | 158 | 261 | 299 | 303 | 244 | 94 |
| Turn Type | Prot | Perm | pm+pt | NA | NA | Perm |
| Protected Phases | 4 |  | 5 | 2 | 6 |  |
| Permitted Phases |  | 4 | 2 |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 9.0 | 30.0 | 30.0 | 30.0 |
| Total Split (s) | 27.0 | 27.0 | 21.0 | 63.0 | 42.0 | 42.0 |
| Total Split (\%) | 30.0\% | 30.0\% | 23.3\% | 70.0\% | 46.7\% | 46.7\% |
| Yellow Time (s) | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  | Lead |  | Lag | Lag |
| Lead-Lag Optimize? |  |  | Yes |  | Yes | Yes |
| Recall Mode | None | None | None | Max | Max | Max |
| v/c Ratio | 0.56 | 0.56 | 0.36 | 0.24 | 0.26 | 0.11 |
| Control Delay | 40.0 | 9.3 | 5.6 | 5.5 | 13.2 | 3.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 40.0 | 9.3 | 5.6 | 5.5 | 13.2 | 3.5 |
| Queue Length 50th (m) | 24.3 | 0.0 | 13.3 | 14.9 | 20.4 | 0.0 |
| Queue Length 95th (m) | 37.0 | 11.8 | 23.6 | 25.7 | 37.1 | 6.1 |
| Internal Link Dist (m) | 446.9 |  |  | 844.6 | 1189.7 |  |
| Turn Bay Length (m) |  | 30.0 | 45.0 |  |  | 30.0 |
| Base Capacity (vph) | 453 | 591 | 885 | 1282 | 948 | 851 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.35 | 0.44 | 0.34 | 0.24 | 0.26 | 0.11 |
| Intersection Summary |  |  |  |  |  |  |

Cycle Length: 90
Actuated Cycle Length: 82.1
Natural Cycle: 65
Control Type: Semi Act-Uncoord

Splits and Phases: 17: Fuller Ave \& Robert St E


1145 Fuller Avenue
17: Fuller Ave \& Robert St E

HCM Signalized Intersection Capacity Analysis
Background (2028) AM Peak Hour with Improvements



1145 Fuller Avenue
17: Fuller Ave \& Robert St E

HCM Signalized Intersection Capacity Analysis
Background (2028) PM Peak Hour with Improvements


## Appendix G - <br> Transportation Tomorrow Survey - Excerpt

## 要 datamanagementgroup

Hello John Northcote
Database Index DMG TTS CCP Contact Logout

## TTS Cross Tabulation

## Cross Tabulation Query Form - Trip - 2016 v1.1

## Filter Variables



## Group Attributes

```
Row Grouping Column Grouping Table Grouping
```

Grouping file: Choose File No file chosen

## Filter Selection +



## Output

- Comma-delimited table Column format Expansion Factor On Click to Select Load Load
Execute Query Select All Save As
Wed Nov 072018 19:07:51 GMT-0500 (Eastern Standard Time) - Run Time: 2197ms
Cross Tabulation Query Form - Trip - 2016 v1.1

Row: 2006 GTA zone of destination - gta06_dest
Column: 2006 GTA zone of household - gta06_hhld

## Filters:

(2006 GTA zone of household - gta06_hhld In 8573

Trip purpose of destination - purp_dest In w,r)

Table:
,8573

## TTS Cross Tabulation

## Cross Tabulation Query Form - Trip - 2016 v1.1

## Filter Variables

2006 GTA zone of desti... $\times \geqslant 2006$ GTA zone of hous... $\times \geqslant$ (Optional) Table Altribute $\quad$.

## Group Attributes

| Row Grouping | Column Grouping |
| :--- | :--- |

Grouping file: Choose File No file chosen

## Filter Selection +

2006 GTA zone of household

## Output

Comma-delimited table Column format Expansion Factor On Click to Select Load Load
Execute Query Select All Save As
Wed Nov 072018 19:07:51 GMT-0500 (Eastern Standard Time) - Run Time: 2197ms
Cross Tabulation Query Form - Trip - 2016 v1.1
Row: 2006 GTA zone of destination - gta06_dest
Column: 2006 GTA zone of household - gta06_hhld
Filters:
( 2006 GTA zone of household - gta06_hhld In 8573
and
Start time of trip - start_time In 700-900
and
Trip purpose of destination - purp_dest In $w, r$ )

## Appendix HSynchro Analysis Output Total Traffic Volumes

|  | 4 | $\rightarrow$ | $\cdots$ | 7 | $4$ | 4 | 4 | $\dagger$ | $p$ |  | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | \$ |  |  | \& |  |  | \$ |  |
| Traffic Volume (veh/h) | 8 | 2 | 48 | 51 | 4 | 2 | 13 | 395 | 20 | 1 | 137 | 2 |
| Future Volume (Veh/h) | 8 | 2 | 48 | 51 | 4 | 2 | 13 | 395 | 20 | 1 | 137 | 2 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 |
| Hourly flow rate (vph) | 11 | 3 | 67 | 71 | 6 | 3 | 18 | 549 | 28 | 1 | 190 | 3 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 798 | 806 | 192 | 861 | 794 | 563 | 193 |  |  | 577 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 798 | 806 | 192 | 861 | 794 | 563 | 193 |  |  | 577 |  |  |
| tC , single (s) | 7.4 | 7.5 | 6.2 | 7.1 | 7.5 | 7.2 | 4.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.8 | 4.9 | 3.3 | 3.5 | 4.9 | 4.2 | 2.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 96 | 99 | 92 | 72 | 97 | 99 | 99 |  |  | 100 |  |  |
| cM capacity (veh/h) | 259 | 222 | 848 | 250 | 226 | 379 | 1317 |  |  | 1006 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total | 81 | 80 | 595 | 194 |  |  |  |  |  |  |  |  |
| Volume Left | 11 | 71 | 18 | 1 |  |  |  |  |  |  |  |  |
| Volume Right | 67 | 3 | 28 | 3 |  |  |  |  |  |  |  |  |
| cSH | 600 | 252 | 1317 | 1006 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.13 | 0.32 | 0.01 | 0.00 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 3.7 | 10.5 | 0.3 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 11.9 | 25.8 | 0.4 | 0.1 |  |  |  |  |  |  |  |  |
| Lane LOS | B | D | A | A |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 11.9 | 25.8 | 0.4 | 0.1 |  |  |  |  |  |  |  |  |
| Approach LOS | B | D |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 3.4 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 47.2\% |  | Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |



|  | 4 |  | 4 |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }^{7}$ | 4 | 4 | 7 |
| Traffic Volume (vph) | 143 | 206 | 236 | 256 | 239 | 125 |
| Future Volume (vph) | 143 | 206 | 236 | 256 | 239 | 125 |
| Lane Group Flow (vph) | 181 | 261 | 299 | 324 | 303 | 158 |
| Turn Type | Prot | Perm | pm+pt | NA | NA | Perm |
| Protected Phases | 4 |  | 5 | 2 | 6 |  |
| Permitted Phases |  | 4 | 2 |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 9.0 | 30.0 | 30.0 | 30.0 |
| Total Split (s) | 27.0 | 27.0 | 21.0 | 63.0 | 42.0 | 42.0 |
| Total Split (\%) | 30.0\% | 30.0\% | 23.3\% | 70.0\% | 46.7\% | 46.7\% |
| Yellow Time (s) | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  | Lead |  | Lag | Lag |
| Lead-Lag Optimize? |  |  | Yes |  | Yes | Yes |
| Recall Mode | None | None | None | Max | Max | Max |
| v/c Ratio | 0.61 | 0.55 | 0.39 | 0.26 | 0.33 | 0.18 |
| Control Delay | 41.0 | 8.7 | 6.3 | 6.0 | 14.7 | 3.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 41.0 | 8.7 | 6.3 | 6.0 | 14.7 | 3.2 |
| Queue Length 50th (m) | 28.2 | 0.0 | 14.1 | 17.2 | 27.4 | 0.0 |
| Queue Length 95th (m) | 41.5 | 11.7 | 25.3 | 29.5 | 48.4 | 7.4 |
| Internal Link Dist (m) | 446.9 |  |  | 844.6 | 1189.7 |  |
| Turn Bay Length (m) |  | 30.0 | 45.0 |  |  | 30.0 |
| Base Capacity (vph) | 448 | 588 | 824 | 1268 | 932 | 869 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.40 | 0.44 | 0.36 | 0.26 | 0.33 | 0.18 |
| Intersection Summary |  |  |  |  |  |  |

Cycle Length: 90
Actuated Cycle Length: 83.1
Natural Cycle: 65
Control Type: Semi Act-Uncoord

Splits and Phases: 17: Fuller Ave \& Robert St E




7: Fuller Ave \& Commercial Access





|  | 4 |  | 4 |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 「 | ${ }^{7}$ | 4 | 4 | F |
| Traffic Volume (vph) | 144 | 221 | 266 | 210 | 340 | 289 |
| Future Volume (vph) | 144 | 221 | 266 | 210 | 340 | 289 |
| Lane Group Flow (vph) | 171 | 263 | 317 | 250 | 405 | 344 |
| Turn Type | Prot | Perm | pm+pt | NA | NA | Perm |
| Protected Phases | 4 |  | 5 | 2 | 6 |  |
| Permitted Phases |  | 4 | 2 |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 25.0 | 25.0 | 9.0 | 30.0 | 30.0 | 30.0 |
| Total Split (s) | 27.0 | 27.0 | 21.0 | 63.0 | 42.0 | 42.0 |
| Total Split (\%) | 30.0\% | 30.0\% | 23.3\% | 70.0\% | 46.7\% | 46.7\% |
| Yellow Time (s) | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  | Lead |  | Lag | Lag |
| Lead-Lag Optimize? |  |  | Yes |  | Yes | Yes |
| Recall Mode | None | None | None | Max | Max | Max |
| v/c Ratio | 0.59 | 0.55 | 0.46 | 0.19 | 0.42 | 0.37 |
| Control Delay | 40.4 | 8.8 | 6.8 | 5.4 | 15.7 | 4.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 40.4 | 8.8 | 6.8 | 5.4 | 15.7 | 4.9 |
| Queue Length 50th (m) | 26.5 | 0.0 | 14.5 | 12.1 | 38.4 | 5.8 |
| Queue Length 95th (m) | 42.6 | 15.3 | 27.8 | 23.4 | 70.1 | 20.5 |
| Internal Link Dist (m) | 446.9 |  |  | 844.6 | 1189.7 |  |
| Turn Bay Length (m) |  | 30.0 | 45.0 |  |  | 30.0 |
| Base Capacity (vph) | 460 | 603 | 758 | 1289 | 953 | 934 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.37 | 0.44 | 0.42 | 0.19 | 0.42 | 0.37 |
| Intersection Summary |  |  |  |  |  |  |

Cycle Length: 90
Actuated Cycle Length: 82.5
Natural Cycle: 65
Control Type: Semi Act-Uncoord

Splits and Phases: 17: Fuller Ave \& Robert St E




7: Fuller Ave \& Commercial Access



